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## RESEARCH ARTICLE

# Spaceborne miniaturized UHF dual band helix antenna with a small frequency ratio

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## Abstract

This study proposes a novel miniaturized circularly polarized (CP) ultrahigh frequency (UHF) quadrifilar helix antenna for spaceborne applications. The dual-band operation is realized using four inverted-U shaped helical strips (IUSHs) that are rotated and alternately arranged on the four faces of a hollow polyimide cuboid in a sequential rotation manner, which effectively reduces the size of the antenna. Furthermore, the four IUSHs are connected by a cross-shape strip at the top of the antenna to control the dual resonant frequencies, resulting in a small dual-band frequency ratio. The proposed antenna is both lightweight

and robust when compared with the conventional miniaturized CP antennas operating at similar bands with similar performance. In particular, its compact radiator provides effective miniaturized spaceborne solution without the need of high-dielectric coefficient materials. A device for spaceborne application that operates at 402/505 MHz is designed, fabricated, measured, and in-orbit tested with a weight of 651 g and an effective size of  $0.161 \times 0.161 \times 0.228 \lambda_{402\text{MHz}}^3$  ( $\lambda_{402\text{MHz}}$  is the wavelength at 402 MHz). The measured gain and axial ratio of the proposed antenna are better than 5.32 dBi and 2.18 dB, respectively, within 2 and 12 MHz bandwidth for the two bands. The test results proved that the methods used to design the proposed antenna are effective.

## KEYWORDS

dual-band operation, quadrifilar helix antenna, small frequency ratio, spaceborne, UHF band

## 1 | INTRODUCTION

Ultrahigh frequency (UHF) bands cover a frequency range of 0.3–1 GHz according to IEEE standards. Although inherently low in data rate, spaceborne UHF datalinks are expected to be operationally available for a long time, as the EM wave of the band can easily penetrate obstacles, thereby providing a stable wireless linkage.<sup>1,2</sup>

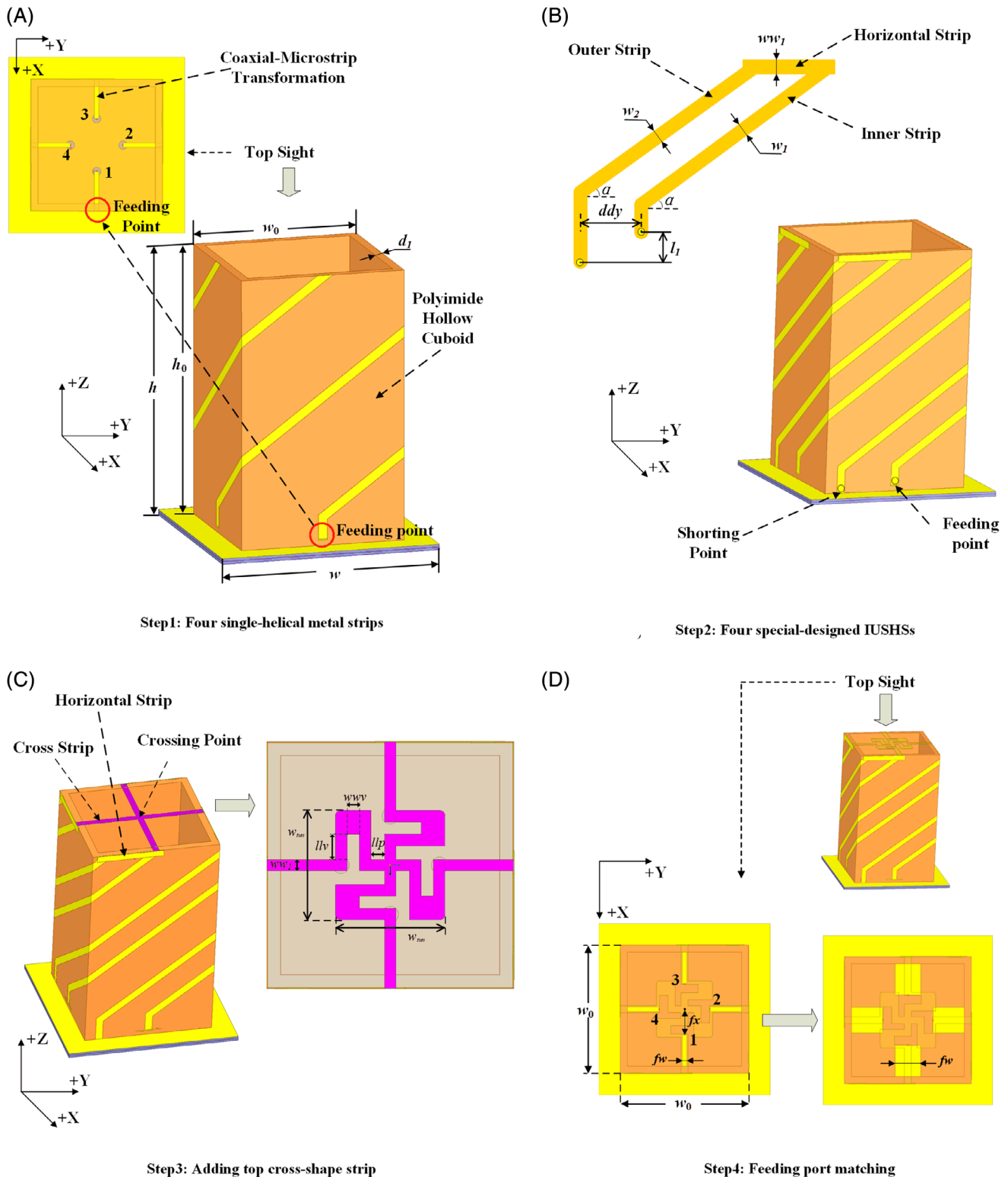
Quadrifilar helical antennas (QHAs) with circularly polarized (CP) radiation are widely used in tracking telemetry and command (TT&C), satellite navigation systems, and data collection systems (DCSs). Presently, with the DCS development of low earth orbit microsatellites, wide hemispherical beamwidths, and a small frequency ratio are generally required for spaceborne antenna applications. However, conventional miniaturized QHAs endure narrow bandwidths and ill-matched input impedances because of their operation at resonant modes instead of traveling modes.<sup>3,4</sup>

This study proposes an innovative miniaturized QHA for a small/micro satellite to satisfy the specifications: operating frequency of 401–403 MHz, 499–511 MHz; 3 dB-axial-ratio beamwidth of  $-60^\circ \leq \theta \leq 60^\circ$  (LHCP); gain of  $\geq 3$  dBi at broadside,  $\geq -2.5$  dBi at  $-60^\circ \leq \theta \leq 60^\circ$ ;  $\leq 0.142 \times 0.142 \times 0.211 \lambda_{402\text{MHz}}^3$  ( $\lambda_{402\text{MHz}}$  is the wavelength at 402 MHz), or  $\leq 106 \times 106 \times 157 \text{ mm}^3$ . A compact electrical size of 0.142

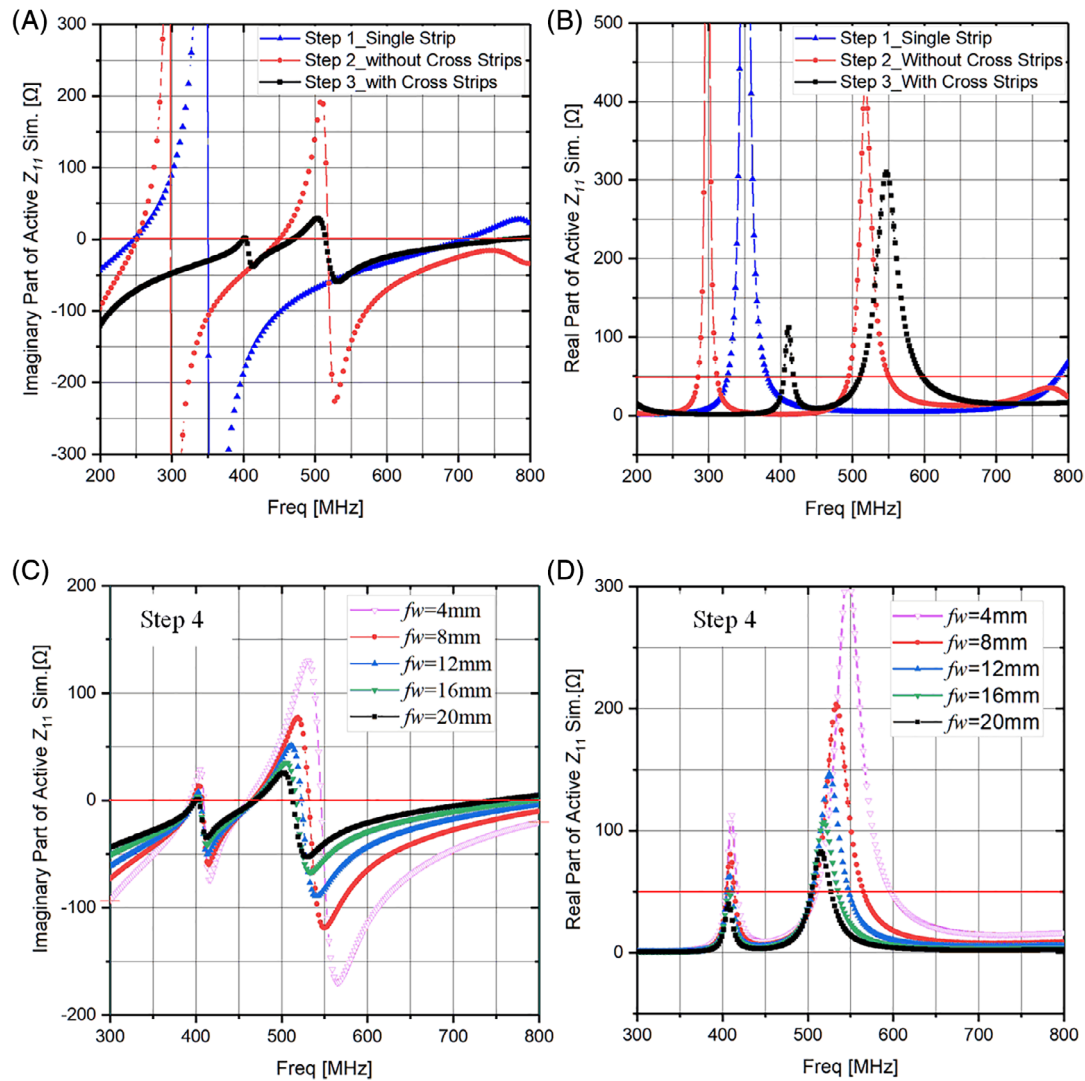
$\lambda_{402\text{MHz}}$  and a low dual-band frequency ratio of 1.25 attribute to the complex design.

Various miniaturized QHAs based on dielectric loading insertion,<sup>5</sup> application of different helix turn angles,<sup>6</sup> helix

antenna arms folding,<sup>7</sup> inverted-F monopoles folding,<sup>8</sup> and power divider networks<sup>9</sup> have been proposed. However, miniaturization constricts the bandwidth. To overcome this drawback, addition of a parasitic helix arm to broaden the bandwidth,<sup>10-13</sup>



**FIGURE 1** Evolution steps of proposed QHA: (A) Four single-helical metal strips; (B) Four special designed IUSHSs; (C) Adding top cross-shape strip; and (D) Feeding port matching. ( $w_0 = 90$  mm,  $h_0 = 149$  mm,  $d_1 = 5$  mm,  $\alpha = 35^\circ$ ,  $dd = 39$  mm,  $l_1 = 10$  mm,  $fw = 19$  mm,  $w_1 = 7$  mm,  $ww_1 = 5$  mm,  $w_2 = 5$  mm,  $w_{2ar} = 39.5$  mm). IUSHS, inverted-U shaped helical strips; QHA, quadrifilar helical antennas [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

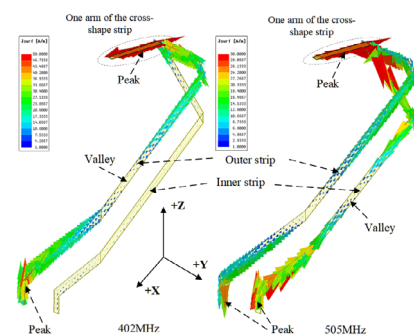


**FIGURE 2** Simulated imaginary and real parts of Active  $Z_{11}$ : (A)  $\text{Im}[\text{Active } Z_{11}]$  of steps 1–3. (B)  $\text{Re}[\text{Active } Z_{11}]$  of steps 1–3. (C)  $\text{Im}[\text{Active } Z_{11}]$  under different  $f_w$  (step 4). (D)  $\text{Re}[\text{Active } Z_{11}]$  under different  $f_w$  (step 4) [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

use of stepped-width arms,<sup>14</sup> or use of a dual-faced slot radiation structure<sup>15</sup> to realize dual-band operation are proposed. Nevertheless, the performance cannot be satisfied using these designs. Therefore, this study focuses on implementing innovative designs. Specifically, it aims to design a spaceborne miniaturized UHF dual-band antenna to overcome existing challenges.

## 2 | DESIGN OF THE ANTENNA

QHA is a circular polarization (CP) antenna, which is widely used in spaceborne applications. It primarily consists of a four-element radiator and a feeding network. The radiator is generally constructed using helical conducting strips on a dielectric substrate.<sup>12,13</sup> The feeding network provides a multiway signal with an equal amplitude and a progressive phase shift to drive the radiator. Miniaturized QHA is a resonant antenna. Therefore, its dimensions must be selected appropriately to obtain optimum characteristics in its operating frequency band.



**FIGURE 3** Resonance mode on the combination of cross-shape strip and IUSHS at 402/505 MHz (current distribution). IUSHS, inverted-U shaped helical strips [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

### 2.1 | Radiator design and experiments

In this section, a miniaturized radiator is presented and discussed, which utilizes four inverted-U shaped helical strips (IUSHSs) to reduce the size and operate at the dual band as

well as a cross-shaped strip between the four IUSHSs to reduce the resonant frequency ratio. The evolution of the design is described below.

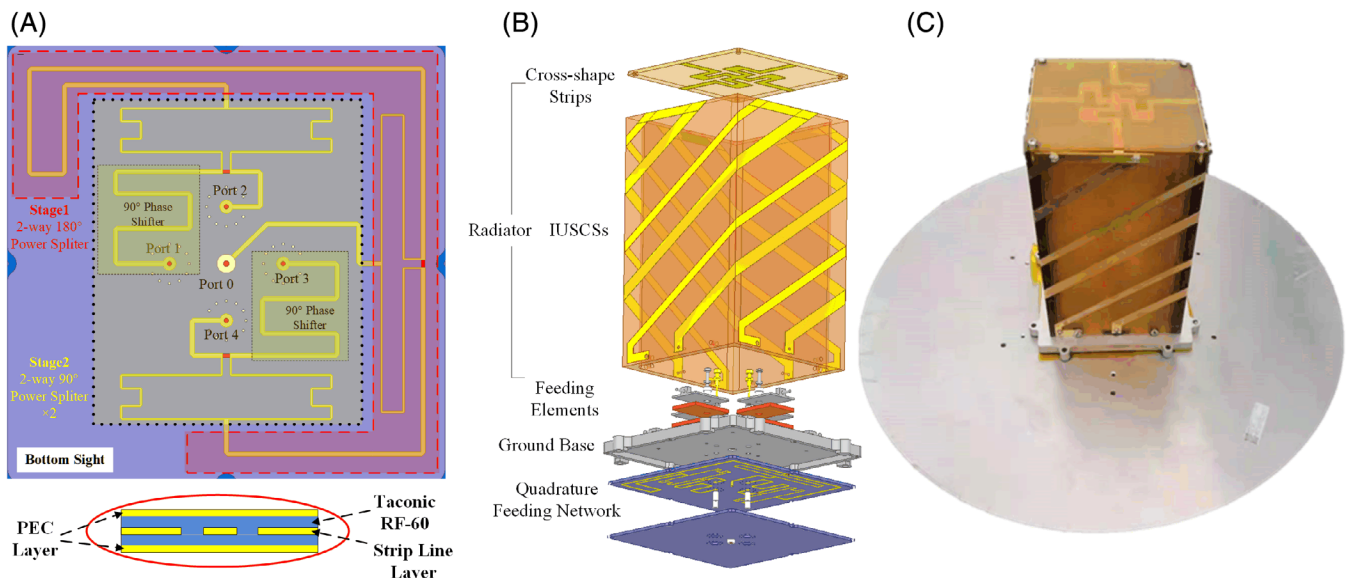
The structural dimension requirement of the proposed QHA is shown in Figure 1(A). The radiator is composed of four IUSHSs, which are wound as four helices on a supporting hollow cuboid polyimide frame with limited side length  $w \leq 106$  mm, height  $h \leq 157$  mm. For an electrically small antenna, the larger the size, the better the performance. The proposed QHA is designed according to the maximum acceptable size,  $w = 106$  mm,  $h = 157$  mm, and frame thickness  $d_1 = 5$  mm.

Initially (step 1), a traditional miniaturized QHA radiator was designed, as shown in Figure 1(A). It forms four straight helical strips, where each strip has approximately  $\lambda/4$  and  $1/2$  turn, with an opening at the top. The feeding point is arranged at the center of the bottom edge of the cuboid flank. The resonance point is defined as the frequency at which the imaginary part of the input impedance ( $\text{Im}[\text{Active } Z_{11}]$ ) is zero and the real part ( $\text{Re}[\text{Active } Z_{11}]$ ) is none zero. Simulated  $\text{Im}[\text{Active } Z_{11}]$  is shown in Figure 2(A). A resonant point is observed at 240 and 700 MHz with a frequency ratio of 2.91. Furthermore,  $\text{Re}[\text{Active } Z_{11}]$  is much larger than  $50 \Omega$ , and  $\text{Im}[\text{Active } Z_{11}]$  changes rapidly with frequency (Figure 2(B)), resulting in a poor match at resonant points.

Subsequently (step 2), to realize dual-band operation, an unconventional helical conducting strip, IUSHS, is designed. The expanded view of an IUSHS is shown in Figure 1(B). Each IUSHS with inclination angle  $\alpha$ , is fed with a coaxial port at one end, followed by an elongation and  $180^\circ$  rotation at the other end; it is then shorted to the ground near the feeding point. The elongated and original parts are parallel. Briefly, each rotated metal

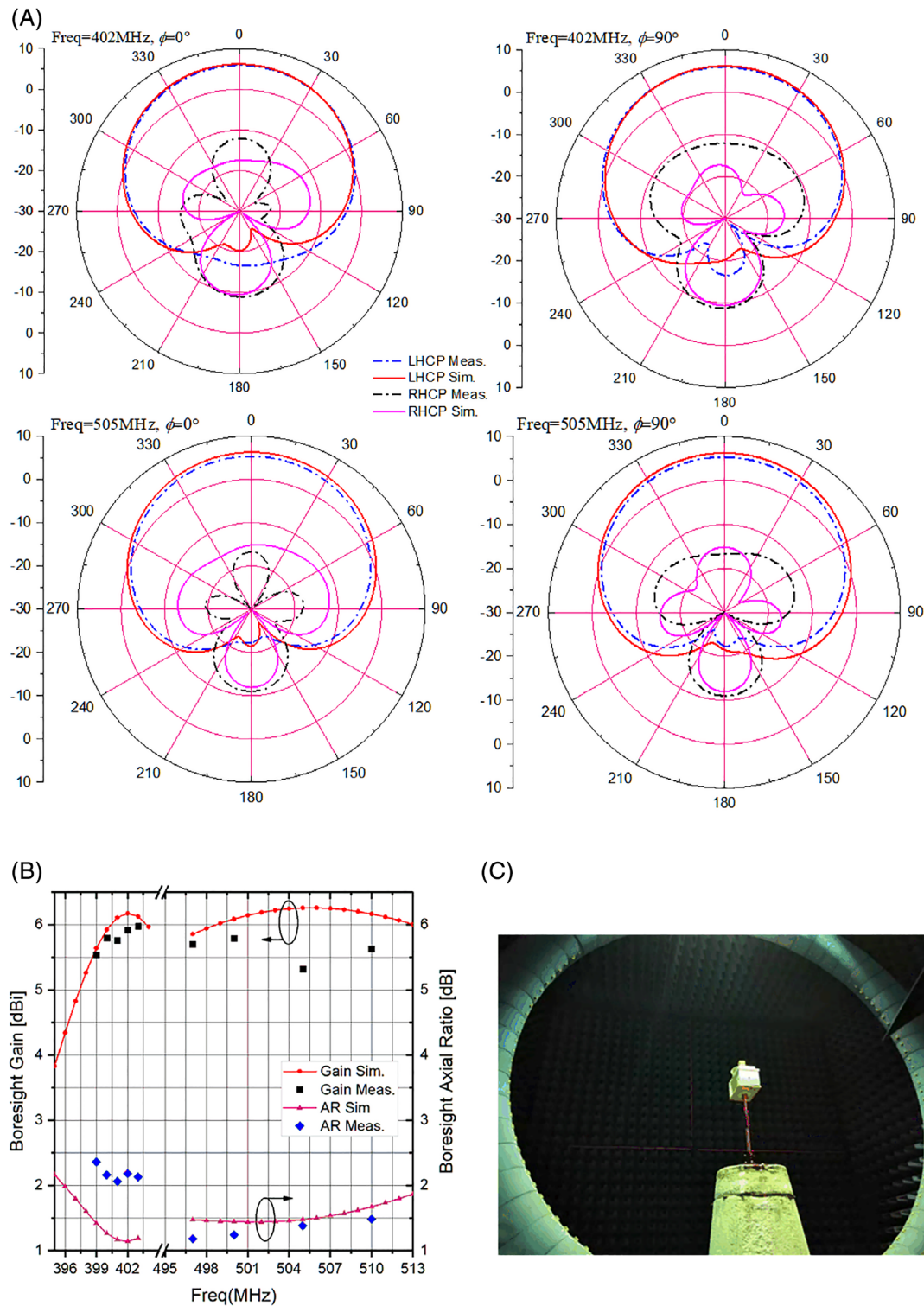
strip consists of an inner strip, an outer strip, and a horizontal strip with widths  $w_1$ ,  $w_2$ , and  $ww_1$ , respectively. The horizontal and vertical distances between the feeding and shorting points are denoted as  $ddy$  and  $l_1$ . This introduces a resonance point of 298 and 515 MHz, with a frequency ratio of 1.73 (Figure 2(A)). However, it still does not satisfy the requirement, and  $\text{Re}[\text{Active } Z_{11}]$  is far from  $50 \Omega$  (Figure 2(B)), resulting in a poor match.

To effectively reduce the frequency ratio, a cross-shaped strip is connected to the horizontal strip of the separated IUSHSs at the top (step 3), as shown in Figure 1(C). The center of the cross-shaped strip is equivalently shorted to the ground, as the phase difference between each two separated IUSHSs is  $180^\circ$ . From Figure 3, the simulated current distributions on an IUSHS shows two different resonant energy distributions at 402 and 505 MHz: one is primarily at the outer strip, while the other is at both strips. Consequently, the resonant points can be tuned independently, to compensate frequency deviation caused by fabrication errors. The current density distribution on the combination of cross-shape strip and IUSHS operates in dual  $\lambda/4$  resonant mode, as shown in Figure 3. Hence, the dimensions of the cross-shape strip will affect the resonant frequency of the radiator. Correspondingly, the geometry dimension of the cross-shape strip is as shown in Figure 1(C), where  $wwv = w_{\text{tun}}/2 - ww_1/2 - llp - 2*ww_1$ ,  $llv = llp + ww_1$ ,  $llp = w_{\text{tun}}/10$ . The impact of the parameters  $w_{\text{tun}}$  and  $ww_1$  on the resonant frequencies have been studied. The dual resonant frequencies will increase simultaneously with the increase of  $w_{\text{tun}}$ . While,  $ww_1$  has monotonous impact to the lower resonant frequency without affecting the higher one. Therefore, independent tuning of two frequencies can be realized by appropriately adjusting the



**FIGURE 4** Fabricated prototype. (A) Explosive view of the model. (B) The feeding network. (C) Photograph of the fabricated prototype mounted on a  $\varphi = 350$  mm metal ground. IUSHS, inverted-U shaped helical strips [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]





**FIGURE 5** Radiation characteristics (sim. vs. meas.) and measurement environment. (A) Radiation patterns on  $\phi = 0^\circ/90^\circ$  plane at 402/505 MHz. (B) Broadside gain and AR. (C) Photograph of the prototype under measurement. AR, axial ratio [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

two parameters. Simultaneously, impedance matching is improved; however, the obtained impedance matching is still unsatisfactory (Figure 2(B)).

Finally (step 4), to improve the impedance matching of the radiator, the width of the transforming line between the

feeding point of the element and the coaxial feeding point is optimized as shown in Figure 1(D). It can be seen from Figure 2(C),(D) that  $\text{Re}[\text{Active } Z_{11}]$  reaches  $50 \Omega$  while  $\text{Im}[\text{Active } Z_{11}]$  slightly varies at 402 and 505 MHz, as  $f_w$  varies from 5 to 20 mm.

**TABLE 1** Comparison of the proposed QHA and previously reported QHAs

Reference	Minimum frequency ratio	Broadside gain	Dimension via $\lambda(D*H)$	Dielectric used on radiator
This work	1.256	>5.92 dBi (402 MHz) >5.32 dBi (505 MHz)	$0.142 \times 0.142 \times 0.214 \lambda_{402\text{MHz}}^3$	Polyimide
19	1.284	>4 dBi (1227 MHz) >4 dBi (1575 MHz)	$\varphi 0.11 \times 0.07 \lambda_{1.227\text{GHz}}^3$	F4B
18	1.173	>1.5 dBi at all band	$\varphi 0.152 \times 0.487 \lambda_{1.227\text{GHz}}^3$	Neltec
17	1.529	> -2 dBi (1227 MHz) > -3 dBi (1575 MHz)	$\varphi 0.094 \times 0.471 \lambda_{1.57\text{GHz}}^3$	Al <sub>2</sub> O <sub>3</sub> ceramic
16	1.148	/	$\varphi 0.24 \times 0.56 \lambda_{401\text{MHz}}^3$	No
15	1.284	>4.44 dBi (1227 MHz) >3.87 dBi (1575 MHz)	$\varphi 0.12 \times 0.35 \lambda_{1.227\text{GHz}}^3$	Rogers Duroid 5880
14	1.284	>6.3 dBi (1227 MHz) >6.4 dBi (1575 MHz)	$\varphi 0.18 \times 0.33 \lambda_{1.227\text{GHz}}^3$	PET
12	1.143	>1.75 dBi (1400 MHz) >2.2 dBi (1600 MHz)	$\varphi 0.159 \times 0.610 \lambda_{1.4\text{GHz}}^3$	Neltec
10	1.195	>4.2 dBi (1.14 MHz) >2.1 dBi (1.54 MHz) >1.7 dBi (1.84 MHz)	$\varphi 0.15 \times 0.30 \lambda_{1.227\text{GHz}}^3$	Neltec

## 2.2 | Antenna assembly and consolidation for spaceborne applications

A quadrature feeding network is needed to provide equal amplitude signals with sequential phases of 0°, 90°, 180°, and 270°. As shown in Figure 4(A), it is implemented on two Taconic RF-60 substrates, which consists of two-stage Wilkinson power divider cascaded with phase shifters. Simulation shows that a low insertion loss of approximately 0.2 dB was obtained, and the maximum magnitude and phase imbalance are 0.1 dB and 33.6° respectively. An SMA connector connecting Port 0 of the feeding network is fastened on its back.

The proposed antenna can be assembled by mounting the feeding network on the bottom of the radiator, as shown in Figure 4(B),(C), which has a dimension of  $106 \times 106 \times 157 \text{ mm}^3$  (excluding  $\varphi=350 \text{ mm}$  metal ground) or  $0.142 \times 0.142 \times 0.211 \lambda_{402\text{MHz}}^3$  and a weight of 786 g.

To meet the mechanical, thermal, and radiational reliability requirements in spaceborne applications, an engineering design is realized. The fabricated radiator here is slightly different from that of Figure 1 in that all surface components are assembled by means of screw joints instead of welding, solder joints are fastened by screws before welding, immune-to-radiation polyimide is used to support IUSHs.

## 2.3 | Antenna measurements

The prototype is placed in the center of a  $\varphi = 350 \text{ mm}$  metal ground to emulate the satellite body when measured, as shown in Figure 4(C). The measured reflection coefficient is less than -15 dB at 401–511 MHz, similar to the simulated result of the feeding network.

Subsequently, the measured radiation performance is shown in Figure 5. The measured normalized LHCP (main polarization) radiation patterns at the two bands are in agreement with the simulated ones. Measured broadside gains are 5.92 dBi at 402 MHz and 5.32 dBi at 505 MHz, respectively. It can be observed that they are approximately 0.2 and 0.9 dB lower than the simulated ones. The measured broadside axial ratios (ARs) are higher than 2.18 and 1.38 dB at 402 and 505 MHz, while simulated ones are 1.14 and 1.48 dB. Within 2 and 12 MHz bandwidths at the two bands, measured broadside gains are larger than 5.76 and 5.32 dBi respectively, which are 0.34 and 0.7 dB lower than the simulated ones. For AR, the measured results are 2.18 and 1.48 dB, while simulated ones are 1.19 and 1.74 dB. Measured radiation characteristics are slightly deviated from simulated ones because of the errors from dielectric coefficient, fabrication, and assembling. However, these errors also cause that measured AR is better than simulated one because of the better amplitude and phase imbalance of the fabricated prototype than those of the simulation model. Thus, it can be confirmed that the prototype can well satisfy the requirements presented in the introduction.

Space environment tests on sinusoidal vibration, random vibration, and thermal vacuum cycling were conducted for the fabricated prototype. The measured results show negligible differences between the performances of the antenna system before and after the environmental tests.

## 3 | DISCUSSION

Table 1 compares the proposed QHA and previously reported QHAs: although a few reported QHAs achieve high

performance, they are of large sizes.<sup>12,16-18</sup> Certain reported QHAs are compact, yet their frequency ratios and sizes cannot satisfy the required parameters.<sup>10,14,15,19</sup> Loading IUSHs and the cross-shape strip enables the proposed antenna to achieve high broadside gain, small AR, and compact electrical size with a smaller frequency ratio. Furthermore, it provides cost-effective solutions to spaceborne antennas by avoiding dependence on space-specific dielectric materials to realize miniaturization. Consequently, the proposed antenna is a good candidate for spaceborne DCS applications.

## 4 | CONCLUSION

A novel spaceborne miniaturized CP UHF dual-band QHA with a small frequency ratio was presented. A prototype working at 402/505 MHz was designed, fabricated, measured, and in-orbit tested with a weight of 651 g and an effective size of  $0.161 \times 0.161 \times 0.214 \lambda^3_{402\text{MHz}}$ , with a 1.24 frequency ratio. The measured gain and axial ratio of the proposed QHA were better than 5.32 dBi and 2.18 dB at the operating band. The test results proved that the methods used to design the proposed antenna are effective.

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## DATA AVAILABILITY STATEMENT

Data openly available in a public repository that issues datasets with DOIs

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